AD-A273 255





Application of the HEC Prescriptive Reservoir Model in the Columbia River System

Technical Paper No. 146

May 1993

Approved for Public Release. Distribution Unlimited.

93-29290

Papers in this series have resulted from technical activities of the Hydrologic Engineering Center. Versions of some of these have been published in technical journals or in conference proceedings. The purpose of this series is to make the information available for use in the Center's training program and for distribution within the Corps of Engineers

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names doe. not constitute an official endorsement or approval of the use of such commercial products.

Acces	on For						
DTIC	iou, ped	*					
By Dist ib	By Dist ib tio /						
A	Availability Codes						
Dist	Avail and Special	l or					
A-1							

Application of the HEC Prescriptive Reservoir Model in the Columbia River System

By Richard Hayes¹, Michael Burnham¹, and David Ford²

Abstract

The water resources of Columbia River system provide significant hydropower, water supply, flood control, recreation, fishery and navigation benefits to the residents of the Pacific Northwest. Increasingly, the competition among the users of the Columbia system has been intensified by declining fishery resources. The Corps of Engineers (Corps), U.S. Bureau of Reclamation (Reclamation) and Bonneville Power Administration (BPA) are jointly conducting a review of fourteen federal projects within the Columbia basin. This effort has been termed the Columbia River System Operation Review (SOR). To provide the Corps SOR study team with a basis for more optimal allocation of system resources, the Hydrologic Engineering Center (HEC) has applied the recently developed Prescriptive Reservoir Model, HEC-PRM, to the major reservoirs of the Columbia River system upstream of Bonneville Dam.

The HEC-PRM represents the Columbia system as a link-node network and uses network-flow programming to optimize, in time and space, flow and storage in the system. The representation of operational goals in HEC-PRM is accomplished through flow, storage and energy economic penalty functions. Operational purposes represented by penalty functions included hydropower, water supply, flood control, navigation, recreation, and anadromous fish. The application was based on fifty year period-of-record with a monthly time interval. The HEC data storage system, HEC-DSS, was utilized extensively for data management and analysis of results.

This paper summarizes the interim findings of the second phase of this ongoing application.

System Description

The Columbia River basin embraces approximately 259,000 sq. mi. (670,000 sq. km.) of the Pacific Northwest from Canadian Province of British Columbia in the north to

Hydraulic Engineer and Chief of Planning, Respectively, US Army Corps of Engineers, Water Resources Support Center, Hydrologic Engineering Center, Davis, CA.

² Engineering Consultant, Sacramento, CA.

northern Nevada at its most southern point, and from the Pacific Ocean on the west to Wyoming on the east. Major storage and run-of-river reservoirs on the Columbia and its major tributaries (the Kootenai, Pend Oreille, Snake and Clearwater Rivers) are shown in Figure 1.

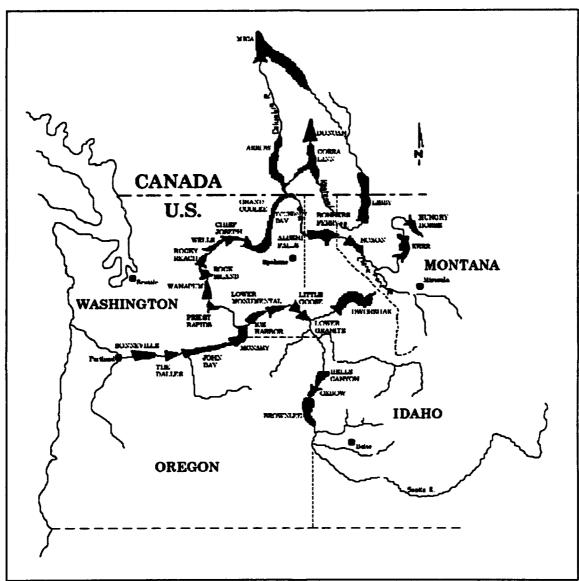


Figure 1 Columbia River System

Average annual runoff is about 275,000 cfs (7,790 cms), of which 25 percent comes from Canada. Precipitation varies from an annual total of over 100 inches near Mica in British Columbia and along Cascade Range at the basins western boundary to about 6 inches in southern Idaho and central Washington. Runoff from the basin above Bonneville Dam has a strong seasonal pattern with most runoff resulting from snowmelt in April through July.

Water Resources Development

Development of federal reservoirs along the main stem of the Columbia began in the 1930's primarily as consequence of nationwide unemployment during the Great Depression. Bonneville, a Corps navigation and hydropower project, was begun by the Works Progress Administration and was completed by the Corps in 1938. Grand Coulee, Reclamation's mainstem Columbia irrigation and hydropower project, went in service in 1941. Energy from both projects contributed significantly to the regions rapid industrial growth during World War II.

During the 1950's the Corps completed The Dalles, McNary, and Chief Joseph on the Columbia and Albeni Falls on the Pend Oreille River. Reclamation added Hungry Horse Reservoir on the Flathead River to the federal system in 1952. During the 1960's the Corps continued development of the Columbia-Snake River Waterway navigation system by finishing John Day on the Columbia and Ice Harbor and Lower Monumental on the lower Snake River. Corps development in the Snake River basin continued in the 1970's with Little Goose and Lower Granite on the Snake River and Dworshak on the North Fork of Clearwater River.

In January 1961, the United States and Canada became signatories to the Columbia River Treaty. The treaty provided for cooperative development of four storage projects to be operated for flood control and hydropower: Libby in Montana; and Mica, Arrow, and Duncan in British Columbia. Duncan, the first of the Canadian Treaty projects was completed in 1967; Arrow (Hugh Keenleyside) was completed in 1968; and, Mica was completed in 1973. In 1975, the Corps completed Libby Dam, the fourteenth federal reservoir included in the ongoing System Operation Review (SOR) investigations.

In addition to the major federal and treaty projects, numerous other reservoirs have been developed throughout the system principally for hydropower and irrigation. The Columbia River Basin Master Water Control Manual (USACE,1984) indicates that the Columbia Basin above its mouth includes 211 water control projects with a storage greater than 5,000 acre-feet or installed capacity of 5 mW or more.

The Problem

While reservoir projects within the Columbia Basin have provided significant flood control, irrigation, hydropower, recreation and navigation benefits for the region the cumulative effect of these works coupled with pollution, over harvesting, and other habitat changes have had an impact on the Columbia River fishery. According to the Master Water Control Manual, the 1911 harvest of Columbia River salmon and steelhead was about 50 million pounds. This figure has been estimated to be approximately the natural sustainable annual yield. The 1911 harvest stands in sharp contrast to the 10 million pound harvest in 1989 cited in The Columbia River System: The Inside Story (Interagency Team, 1991). The federal agencies and the fish and wildlife departments of Idaho,

Oregon and Washington have invested heavily in physical facilities including fish hatcheries, ladders, screens and bypass facilities.

Operation modifications to aid the downstream migration of juvenile salmon and steelhead including provisions for increased springtime flows and spillway discharges are being utilized. Still other operation alternatives involving seasonal storage drawdowns, primarily on the navigation impoundments of the lower Snake River and increased flows from upstream storage reservoirs have been proposed. Operational or physical modifications to meet changing demands or enhance any of the uses at the various reservoirs and stream reaches of Columbia River will in all likelihood impact to some degree one or more of the other system uses.

The problems of operating the coordinated system of flood control and hydropower reservoirs by BPA, the Corps, and Reclamation are summarized in The Columbia River: A System Under Stress (BPA, USACE, BuRec, 1990) in which they state:

Growth in our region, along with changing priorities, are putting our river system increasingly under stress. There simply is not enough water flowing in the system to meet all the demands. Trade-off must be considered ... in recent years, demands by the various users of the river have increased dramatically, resulting in increasing conflicts among uses.

Consequently, in 1990 the North Pacific Division (NPD) of the Corps of Engineers proposed the interagency system operation review. To assist in the evaluation of the system and the analysis of potential trade-offs NPD requested the Hydrologic Engineering Center to provide technical assistance in the further development and application of the Center's reservoir system optimization model, HEC-PRM.

HEC-PRM

The HEC has recently developed a prescriptive reservoir model to assist in the analysis of Corps reservoir systems. This new model has been termed HEC-PRM (USACE, 1991a). The term "prescriptive" may be explained in part by comparison with the characteristics of another HEC reservoir system model, the widely applied HEC-5 (USACE, 1982a). HEC-5 is classified as a "descriptive" reservoir model. Both types of models are similar in that they require a sequence of flows and link-node descriptions for continuity of flow. In a descriptive model, like HEC-5, operation policies are specified as storage rule curves, channel capacities, hydropower energy demands, diversions and flow requirements. The outcome of an HEC-5 simulation is typically a time series of flows, stages, and energy production which is obtained by following a specified operation policy. The evaluation of specified operation policies to select the "optimal" among those simulated is left to the model user.

HEC-PRM, on the other hand, uses as a formal objective function the minimization of total system cost. The model uses a network flow solver developed by Jensen and Bhaumik (1974) to determine the optimal distribution of flow, storage and energy production in space and time. The primary input to the HEC-PRM model are "penalty" functions, which relate the consequence (cost) of flow, storage and energy production in a system, and a network description to provide the basis for continuity as flow moves through a system of links and nodes. The penalty functions provide an economic basis for operation prioritization. The model automatically nominates alternative policies which it evaluates with a built-in simulation module. Feasible alternatives are evaluated until a minimum cost policy is determined.

For convenience, HEC-PRM input penalty functions and flow sequences, as well as optimized flows and storages, are handled with HEC-DSS (USACE, 1990). The HEC-DSS utility programs DSSMATH, DSSUTL and DSPLAY are used to develop, manage and plot time series data. Two HEC-PRM utility programs PENF (a graphical penalty function editor) and PRMPP (a post processor) are currently being developed and tested.

Columbia River HEC-PRM Application

HEC-PRM was demonstrated to be an appropriate tool for the analysis of reservoirs with its first application on the Missouri River system. This application for the Corps Missouri River Division (MRD) on the Corps' six mainstem reservoirs was completed in 1990 (USACE, 1991b). The Missouri River system, from the stand point of system optimization, is a relatively straight foreword system with six large tandem reservoirs under the same management. The competing interests in the Missouri system included lake recreation, hydropower production, flood control, water supply and downstream navigation and environmental concerns.

The Corps North Pacific Division (NPD) in 1990 proposed an interagency review of the Columbia River system. The Columbia River, like the Missouri, has recently experienced a system wide water shortage that exacerbated the competition among the various system users. The two systems are similar in that they both have almost the same types of competing interests. The principle exception being in the Missouri system the major environmental concern is maintenance of steady flows for sand bar nesting birds; whereas, the major environmental concern of the Columbia system is the maintenance of seasonal flows to aid the downstream migration salmon and steelhead.

The NPD, as a part of the SOR requested HEC to test the applicability of HEC-PRM to the more complex and larger Columbia River system. This effort, termed Phase I, was initiated in and completed in 1991. It was anticipated that a second phase would follow with more economic detail if the Phase I application proved successful. The findings of the Phase I of the application are reported in Columbia River System Analysis Model - Phase I (USACE, 1991b). The results of the Phase I application verified the applicability of HEC-PRM to a complex system such as the Columbia. It was determined

that the HEC would proceed with the second phase of the analysis. It was agreed that this effort would include the following: expansion of the network to include more storage reservoirs; enhancements to the HEC-PRM hydropower analysis capability; analysis of several alternatives; and a workshop to transfer the technology the Corps SOR team.

HEC began the second phase of the application in fall of 1991. The Phase II network configuration is shown in Figure 2. The network includes fourteen storage reservoirs, five run-of-river (pondage) reservoirs and three non-reservoir locations.

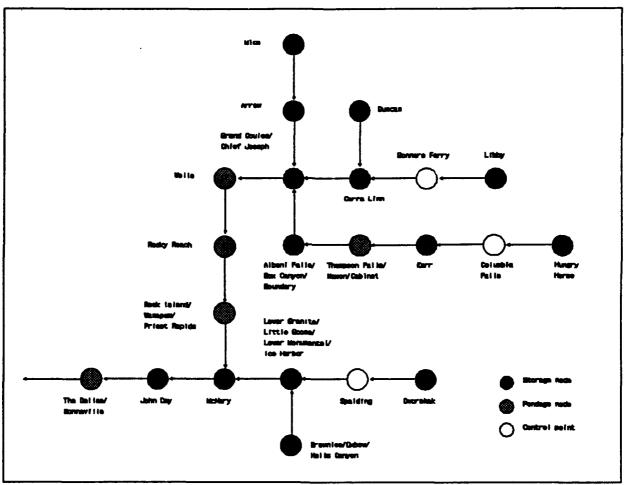


Figure 2 Single-period Network Model of Columbia River System

During the Phase I application it was noted that HEC-PRM storages for Corra Linn (Lake Kootenay), a Canadian hydropower project on the Kootenay River, did not correspond to the simulation results of NPD's HYSSR (USACE,1982b) simulation model to the degree deemed reasonable. Upon investigation is was determined that Corra Linn did not have sufficient outlet capacity to prevent storage from exceeding upper storage

limit. It was further determined that two other reservoirs in the system could also exhibit the same characteristic. The other two are Kerr (Flathead Lake) and Albeni Falls (Lake Pend Oreille). All three are similar in that they are control structures located on a river reach some distance from a natural lake. In order to model these reservoirs, the nominal upper storage was raised to an arbitrarily high value and a restrictive maximum flow limit was specified. To discourage HEC-PRM from utilizing this zone in other than a flood condition, the reservoir storage penalties were modified to inflict a relatively high cost for storage above the nominal full pool. The results obtained have been determined to be appropriate for the current application. It is anticipated that polices determined with HEC-PRM will be modeled with a simulation model, in this case HYSSR, which can provide the additional operational details. Reservoir storage and flow limits are shown in Table 1.

Table 1
Columbia River System Storage and Release Limits

	Storage Limits, 1000 Acre-Feet		Release L	imits - CFS
Reservoir	<u>Minimum</u>	Maximum	Minimum	<u>Maximum</u>
Libby	889.9	5,869.4	3,000	_
Corra Linn	144.0	9,999.0		55,940
Duncan	30.0	1,398.6	100	-
Hungry Horse	486.0	3,647.1	400	-
Kerr	572.3	9,999.0	1,500	54,930
Albeni Falls	446.4	9,999.0		129,800
Dworshak	1,452.2	3,468.0	1,000	
Brownlee	431.7	1,426.7	5,000	-
Granite	144.0	1,825.0	-	_
Mica (Alts. 1 & 2)	13,075.0	20,075.0		
Mica (Alt. 3)	8,000.0	20,075.0		
Arrow	227.0	7,327.0	5,000	
Grand Coulee	3,879.0	9,107.4	-	-
McNary	1,170.0	1,350.0		_
John Day	1,989.0	2,523.0		

Penalty functions are the "guiding light" with which HEC-PRM determines the optimal distribution of flow and storage in time and space. For the Columbia River application, penalty functions represented the following six types of system uses: hydropower; flood control; navigation; anadromous fish; water supply; and, recreation.

The hydropower penalty function is expressed in terms of both flow and variable storage. Each of the other uses were expressed in terms of a flow penalty in \$/kaf (1,000's acre feet per month) or a storage penalty in \$/kaf. Penalty functions are varied monthly to reflect the seasonal nature of the various purposes. At each location, the various penalty functions are combined to create a composite function for each month. HEC-PRM requires that all penalties must be piecewise linear convex functions. Figure 3 shows how penalty functions are combined and how an approximate edited function is determined to satisfy the convex requirement.

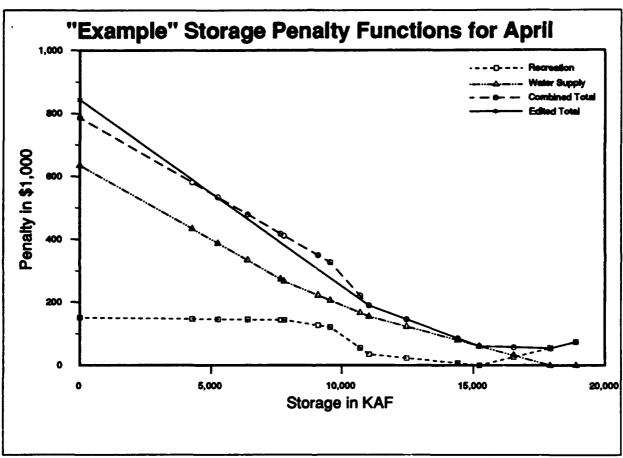


Figure 3 How Penalty Functions are Combined and Approximated

Economic data to create the necessary penalty functions was developed by Corps economists, planners, and engineers from NPD and the Division's Seattle, Portland and Walla Walla Districts under the direction of the Corps Institute for Water Resources (IWR). These data are documented in "Economic Value Functions for Columbia River System Analysis Model, Phase I (Draft)", (USACE, 1992). A graphical penalty function editor (PENF), which was developed during this phase, was used to develop the edited penalty functions. Economic data to develop penalty functions for the Canadian Treaty

reservoirs (Mica, Arrow and Duncan) were not available for use in this phase. Table 2 indicates the purposes which were represented by economic penalty functions throughout the network.

Analysis Overview

The operation for the system was based on flows for the period of 1928 to 1978. Monthly flow data for this period, adjusted to a consistent level of development (1980) were provided by NPD (USACE, 1983). Irrigation depletions, returns and reservoir evaporation were accounted for in the flow data. Irrigation withdrawals from Grand Coulee to Bureau of Reclamation's Columbia Basin Project were treated as a fixed exersion (e.g. not optimized). Three system operation scenarios were selected for analysis, they were: Alternative 1, existing storage allocations with optimization for all operation purposes; Alternative 2, existing storage allocations without optimization for hydropower; and Alternative 3, five million acre-feet of additional storage in Mica, optimization for all operation purposes.

To evaluate system performance of all alternatives with a consistent frame of reference, which represented the present system with current rules and objectives, the results of NPD's continuous HYSSR simulation (SOR base case) were utilized. To provide a valid economic comparison, HYSSR flows and storages were applied to HEC-PRM storage, flow and hydropower penalty functions.

The analyses were performed on a 25 mHz 80486 MS-DOS personal computer with 16 mb memory. The current version of HEC-PRM utilizes allocatable arrays and virtual memory management, which make it extremely accommodating from a users point of view. Execution times for Alternatives 1 and 3 (about 150,000 simultaneous linear equations) for the 50 years of record were about fourteen hours each. For alternative 2, which did not optimize for hydropower, about three hours of execution time was required. Analyses for shorter time spans took significantly less execution time. It is worthwhile to note that for the Columbia system, which has a relatively small amount of storage compared to the annual flow, the presumed requirement to run the entire period of record in a single optimization run is not valid. The analyst has merely to start and end the optimization period at times when the system would be reliably full, which, in the case of the Columbia system, is frequently the case at the end of spring runoff.

To compare the analyses results, performance of all three alternatives and the HYSSR simulation have been computed with the following indices: total system penalty (as computed with HEC-PRM); reliability (the frequency of meeting monthly targets); resiliency (the frequency of recovery after a failure); and vulnerability (the average deviation from the target when a failure occurs).

Table 2
Columbia River System Phase II Network Links and Operation Purposes Penalty Functions

Original	Terminal	Link	0	peration purposes modeled ^s				
Node ¹	Node ¹	Type ²	FC	Hydro	Nav	ImWS	Fish	Rec
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
Libby	Libby	S						_
Libby	Bonners Ferry	н		1				1
Bonners Ferry	Corra Linn	С	1					
Duncan	Duncan	S						
Duncan	Corra Linn	R	1					
Corra Linn	Corra Linn	S	1					
Corra Linn	Coulee	R						
Hungry Horse	Hungry Horse	S						1
Hungry Horse	Columbia Falis	Н		1				
Columbia Falls	Kerr	С	1					
Kerr	Kerr	S	1					
Kerr	Thompson	н	1	1				
Thompson	Thompson	S						
Thompson	Albeni	н		1				
Albeni	Albeni	S	1					1
Albeni	Coulee	Н	✓	1				
Dworshak	Dworshak	S			1			
Dworshak	Spalding	н		•				
Spalding	Granite	С	1					
Brownlee	Brown!ee	S						
Brownlee	Granite	Н						
Granite	Granite	S				1		1
Granite	McNary	Н		•			1	
Mica	Mica	S						
Mica	Arrow	R						
Arrow	Arrow	S						
Arrow	Coulee	R						
Coulee	Coulee	S				•		1
Coulee	Wells	Н						
Wells	Wells	S						
Wells	Rocky Reach	Н						
Rocky Reach	Rocky Reach	S						
Rocky Reach	Rock Island	Н						
Rock Island	Rock Island	S						
Rock Island	McNary	Н						
McNary	McNary	S						
McNary	John Day	Ä		✓				
John Day	John Day	S				1		
John Day	Dalles	H		✓				
Dailes	Dalles	S	_					
Dalles	Sink	Н	1				1	

¹ Refer to Figure 2 for relative location of nodes.

 $^{^2}$ R = simple reservoir-release link; S = storage (period to period) link; H = hydropower reservoir-release link; C = channel-flow link; D = diversion link.

³ FC = flood control; Hydro = hydroelectric-power generation; Nav = navigation; Irr/WS = irrigation and/or water supply; Fish = fish protection; Rec = recreation.

Optimization results contrasting the three alternatives with HYSSR results at Dworshak Reservoir (storage) and The Dalles (flow) are shown in Figures 4 and 5 respectively, for the period of 1928-1938.

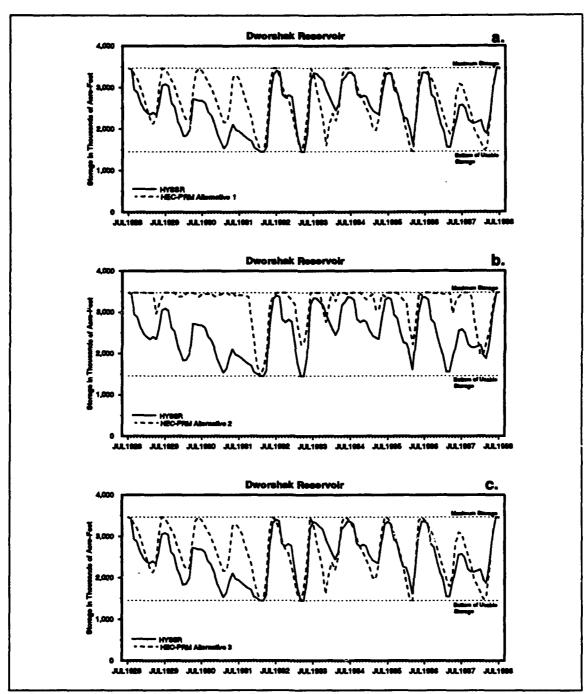


Figure 4 1928-1938 Storage at Dworshak: HYSSR & Alternatives

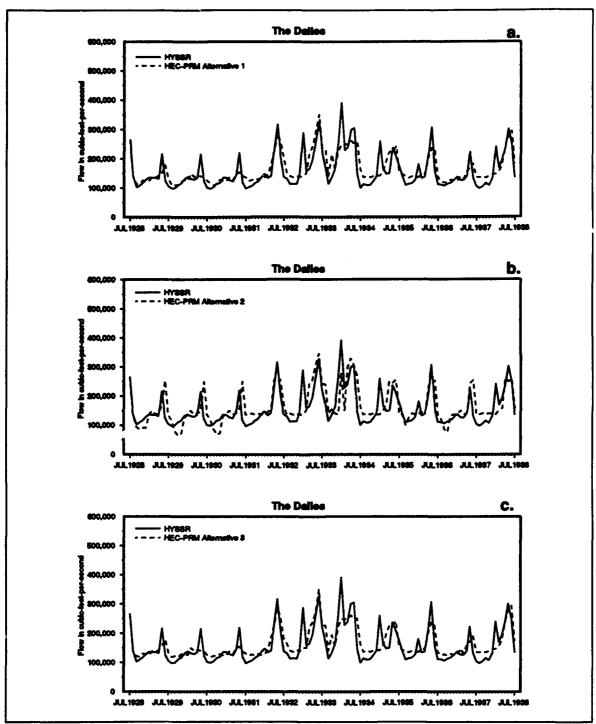


Figure 5 1928-1938 Flow at The Dailes: HYSSR & Alternatives

Study Status

A draft report, Columbia River Reservoir System Analysis: Interim Findings, (Draft), April 1993 has been transmitted to the North Pacific Division for review. It is anticipated that a workshop to transfer the HEC-PRM model and the input files that were developed in this study will be presented to Corps SOR team members in July 1993. At the time of the workshop, it is expected that economic data to develop penalty functions for the Canadian treaty reservoirs may become available. Additional work will be required to develop reservoir operating rules which closely follow the optimal time series of storage and flow, HEC hopes to assist NPD in this effort. The HEC will publish a Phase II report at the conclusion of the study. HEC plans to make a version of HEC-PRM available to the public by the middle of 1993.

Conclusion and Observations

- 1. HEC-PRM has been demonstrated to be capable of period-of-record optimization of complex systems of reservoirs with commonly available computer systems.
- 2. The partially updated Phase I economic data which was the basis for this study should be revisited.
 - 3. Penalty data for the Canadian Treaty reservoirs should be developed.

<u>Acknowledgements</u>

This project was supported by the U.S. Army Corps of Engineers, North Pacific Division and Corps research funds. Dr. David Moser of the Institute for Water Resources guided the development of the economic penalty functions. Dr. Quentin Martin, of the Lower Colorado River Authority, played a key role in the implementation and testing of the HEC-PRM hydropower algorithm. Vladamir Plesa, of the University of California, Davis, developed the PENF and PRMPP programs during the study. Robert Carl, of the Hydrologic Engineering Center (HEC), developed the HEC-PRM computer software, contributed to overall analysis and generated the post processing results. Marilyn Hurst, of HEC, performed data preparation, and analysis of results. Loshan Law, of HEC, typed and assembled the report. Darryl Davis, HEC Director, provided general supervision and guidance for the project.

References

- BPA, USACE, BuRec, (1990). The Columbia river: A system under stress. Portland, OR.
- Interagency Team, (1991), The Columbia River System: The Inside Story, USACE, Portland, OR.
- Jensen, P.A., Bhaumik, G., and Driscoll, B., (1974). "Network flow modeling of multireservoir water distribution systems," CRWR-107, University of Texas, Austin, TX.
- U.S. Army Corps of Engineers, (1982a), HEC-5: Simulation of Flood Control and Conservation Systems, User's Manual. Hydrologic Engineering Center, Davis CA.
- U.S. Army Corps of Engineers, (1982b), HYSSR (Hydro System Seasonal Regulation), Program Users Manual. North Pacific Division, Portland OR.
- U.S. Army Corps of Engineers, (1983), 1980 Level Modified Streamflow, 1828-1978, Columbia River and Coastal Basins. Depletions Task Force, Columbia River Water Management Group, Portland OR.
- U.S. Army Corps of Engineers, (1984), Columbia River Basin, Master Water Control Manual. North Pacific Division, Portland OR.
- U.S. Army Corps of Engineers, (1990), *HEC-DSS User's Guide and Utility Program Manuals*. Hydrologic Engineering Center, Davis CA.
- U.S. Army Corps of Engineers, (1991a), *HECPRM, Hydrologic Engineering Center's Prescriptive Reservoir Model, Program Description*, Hydrologic Engineering Center, Davis, CA.
- U.S. Army Corps of Engineers, (1991b), *Columbia River System Analysis Model Phase I.* Hydrologic Engineering Center, Davis CA.
- U.S. Army Corps of Engineers, (1992), Economic Value Functions for Columbia River System Analysis Model (Draft). Institute for Water Resources, Fort Belvoir, VA.

TECHNICAL PAPER SERIES (\$2 per paper)

TP-1	Use of Interrelated Records to Simulate Streamflow	TP-38 TP-39	Water Quality Evaluation of Aquatic Systems A Nethod for Analyzing Effects of Dam Failure
TP-2	Optimization Techniques for Hydrologic Engineering	TP-40	in Design Studies Storm Drainage and Urban Region Flood Control
TP-3	Methods of Determination of Safe Yield and Compensation Water from Storage Reservoirs	TP-41	Planning HEC-5C, A Simulation Model for System
TP-4	Functional Evaluation of a Water Resources	TP-42	Formulation and Evaluation Optimal Sizing of Urban Flood Control Systems
TP-5	System Streamflow Synthesis for Ungaged Rivers	TP-43	Hydrologic and Economic Simulation of Flood
TP-6	Simulation of Daily Streamflow		Control Aspects of Water Resources Systems
TP-7	Pilot Study for Storage Requirements for Low Flow Augmentation	TP-44	Sizing Flood Control Reservoir Systems by Systems Analysis
TP-8	Worth of Streamflow Data for Project	TP-45	Techniques for Real-Time Operation of Flood
TD-0	Design - A Pilot Study Economic Evaluation of Reservoir System		Control Reservoirs in the Merrimack River
TP-9	Accomplishments	TP-46	Spatial Data Analysis of Nonstructural
TP-10	Hydrologic Simulation in Water-Yield Analysis	TP-47	Measures Comprehensive Flood Plain Studies Using
TP-11	Survey of Programs for Water Surface	17-41	Spetial Data Management Techniques
	Profiles	TP-48	Direct Runoff Hydrograph Parameters Versus
TP-12	Hypothetical Flood Computation for a	TP-49	Urbanization Experience of HEC in Disseminating Information
TP-13	Stream System Maximum Utilization of Scarce Data in	IP-49	on Hydrological Models
	Hydrologic Design	TP-50	Effects of Dam Removal: An Approach to
TP-14			Sedimentation
TP-15	Reservoir Yields Hydrostatistics - Principles of	TP-51	Design of Flood Control Improvements by Systems Analysis: A Case Study
16-13	Application	TP-52	Potential Use of Digital Computer Ground Water
TP-16		.,	Models
	Modeling Techniques	TP-53	Development of Generalized Free Surface Flow
TP-17	Hydrologic Engineering Techniques for Regional Water Resources Planning	TP-54	Models Using Finite Element Techniques Adjustment of Peek Discharge Rates for
TP-18		117"34	Urbenization
	Region	TP-55	The Development and Servicing of Spatial Data
TP-19	Suspended Sediment Discharge in Streams		Management Techniques in the Corps of
TP-20	Computer Determination of Flow Through Bridges	TP-56	Engineers Experiences of the Hydrologic Engineering
TP-21	An Approach to Reservoir Temperature Analysis	1. 30	Center in Maintaining Widely Used Hydrologic and Water Resource Computer Models
TP-22	▼	TP-57	Flood Damage Assessments Using Spetial Data Management Techniques
	Media	TP-58	A Model for Evaluating Runoff-Quality in
TP-23	Uses of Simulation in River Basin Planning		Metropolitan Master Planning
TP-24	Mydroelectric Power Analysis in Reservoir Systems	TP-59	Testing of Several Runoff Models on an Urban Watershed
TP-25 TP-26	Status of Water Resource Systems Analysis	TP-60	Operational Simulation of a Reservoir System
17-20	System Relationships for Panama Canal Water Supply	TP-61	with Pumped Storage Technical Factors in Small Hydropower Plannir
TP-27	System Analysis of the Panama Canal Water Supply	TP-62	Flood Hydrograph and Peak Flow Frequency Analysis
TP-28	Dig tal Simulation of an Existing Water	TP-63	MEC Contribution to Reservoir System Operation
	Resources System	TP-64	Determining Peak-Discharge Frequencies in an
TP-29	Computer Applications in Continuing Education	TP-65	Urbanizing Watershed: A Case Study
TP-30	Drought Severity and Water Supply		Feasibility Analysis in Small Hydropower Planning
TP-31	Dependability Development of System Operation Rules for	TP-66	Reservoir Storage Determination by Computer Simulation of Flood Control and Conservation
11-31	an Existing System by Simulation		Systems
TP-32	Alternative Approaches to Water Resource	TP-67	Hydrologic Land Use Classification Using
	System Simulation	/0	LANDSAT
TP-33	System Simulation for Integrated Use of Hydroelectric and Thermal Power Generation	TP-68	Interactive Monstructural Flood-Control Planning
TP-34	Optimizing Flood Control Allocation for a	TP-69	Critical Water Surface by Minimum Specific
	Multipurpose Reservoir		Energy Using the Parabolic Method
TP-35	Computer Models for Rainfall-Runoff and	TP-70	Corps of Engineers Experience with Automatic
TP-36	River Hydraulic Analysis Evaluation of Drought Effects at Lake	TP-71	Calibration of a Precipitation-Runoff Model Determination of Land Use from Satellite
	Atitian		Imagery for Input to Hydrologic Models
TP-37	Downstream Effects of the Levee	TP-72	Application of the Finite Element Method to
	Overtopping at Wilkes-Barre, PA, During Tropical Storm Agnes		Vertically Stratified Hydrodynamic Flow and Water Quality
	p.,		

TP-73	Flood Mitigation Planning Using HEC-SAM	TP-114	Accu
TP-74	Hydrographs by Single Linear Reservoir Model	TP-115	Appl
TP-75	NEC Activities in Reservoir Analysis		Techi
TP-76	Institutional Support of Water Resource	TP-116	The I
TP-77	Hodels Investigation of Soil Conservation Service	TP-117	HEC-
17-77	Urban Hydrology Techniques	TP-118	Real
TP-78	Potential for Increasing the Output of	,,,	Honor
	Existing Hydroelectric Plants	TP-119	Mult
TP-79	Potential Energy and Capacity Gains from Flood Control Storage Reallocation at	TP-120	PC Techi
	Existing U. S. Hydropower Reservoirs	17-120	Mode
TP-80	Use of Non-Sequential Techniques in the	TP-121	Deve
	Analysis of Power Potential at Storage		Runo
TP-81	Projects Data Management Systems for Water	TP-122	Rive
	Resources Planning	IF ILL	Fore
TP-82	The New HEC-1 Flood Hydrograph Package	TP-123	Deve
TP-83	River and Reservoir Systems Water Quality		Rese
TP-84	Modeling Capability Generalized Real-Time Flood Control System	TP-124	Revie
IP-ON	Model		Prob
TP-85	Operation Policy Analysis: Sam Rayburn	TP-125	An I
	Reservoir		Demo
TP-86	Training the Practitioner: The Hydrologic	TP-126	The '
TP-87	Engineering Center Program Documentation Needs for Water Resources	TP-127	Floor
	Models	TP-128	Two-
TP-88	Reservoir System Regulation for Water	TP-129	State
TP-89	Quality Control A Software System to Aid in Making		Prog
17 07	Real-Time Water Control Decisions	TP-130	Esti
TP-90	Calibration, Verification and Application		Allu
	of a Two-Dimensional Flow Model	TP-131	Hydr
TP-91 TP-92	HEC Software Development and Support Hydrologic Engineering Center Planning	TP-132	Prep
17-72	Hodels	17-132	and :
TP-93	Flood Routing Through a Flat, Complex		Prog
	Flood Plain Using a One-Dimensional	TP-133	Pred
TP-94	Unsteady Flow Computer Program Dredged-Material Disposal Management Model	TP-134	Annu
TP-95	Infiltration and Soil Moisture	TP-135	A Mus
	Redistribution in HEC-1		for I
TP-96	The Hydrologic Engineering Center	TP-136	Pres
TP-97	Experience in Nonstructural Planning Prediction of the Effects of a Flood	TP-137	Miss A Ge
	Control Project on a Meandering Stream	** 131	Syste
TP-98	Evolution in Computer Programs Causes	TP-138	The I
	Evolution in Training Needs: The	TP-139	Issu
TP-99	Hydrologic Engineering Center Experience Reservoir System Analysis for Water	TP-140 TP-141	HEC-
	Quality	TP-142	Syst
TP-100	Probable Maximum Flood Estimation -		Hydr
TD- 101	Eastern United States	TP-143	Runo
1P-101	Use of Computer Program HEC-5 for Water Supply Analysis	TP-144	Agri Revi
TP-102	Role of Calibration in the Application of		Mode
	NEC-6	TP-145	Appl
TP-103	Engineering and Economic Considerations in	4//	Floo
TD-104	Formulating Modeling Water Resources Systems for Water	Tp-146	Appl Mode
,, ,,,,	Quality		
TP-105	Use of a Two-Dimensional Flow Model to		
TD- 104	Quentify Aquetic Habitat		
	Flood-Runoff Forecasting with HEC-1F Dredged-Material Disposal System Capacity		
107	Expension		
TP-108	Role of Small Computers in Two-Dimensional		
TD-100	Flow Modeling		
	One-Dimensional Model For Mud Flows Subdivision Froude Number		
	HEC-5Q: System Water Quality Modeling		
445	Maria Barrata anno de 1800 Barrana de 181 - 1		

TP-112 New Developments in HEC Programs for Floc.

TP-113 Modeling and Managing Water Resource Systems for Water Quality

Control

uracy of Computed Water Surface Profiles cutive Summery ication of Spatial-Data Management nniques in Corps Planning **HEC's Activities in Watershed Modeling** 1 and HEC-2 Applications on the roComputer l-Time Snow Simulation Model for the ongahela River Basin ti-Purpose, Multi-Reservoir Simulation on a hnology Transfer of Corps' Hydrologic elopment, Calibration and Application of off Forecasting Models for the Allegheny er Basin Estimation of Rainfall for Flood ecasting Using Rader and Rain Gage Data eloping and Managing a Comprehensive ervoir Analysis Model ew of the U.S. Army Corps of Engineering olvement With Alluvial Fan Flooding عصه اد Integrated Software Package for Flood ige Analysis Value and Depreciation of Existing ilities: The Case of Reservoirs odolain-Management Plan Enumeration -Dimensional Floodplain Modeling tus and New Capabilities of Computer gram HEC-6: "Scour and Deposition in ers and Reservoirs" mating Sediment Delivery and Yield on uvial Fans rologic Aspects of Flood Warning peredness Program nty-five Years of Developing, Distributing, Supporting Hydrologic Engineering Computer dicting Deposition Patterns in Small Basins ual Extreme Lake Elevations by Total bebility Theorem uskingum-Cunge Channel Flow Routing Method Drainage Networks scriptive Reservoir System Analysis Model souri River System Application eneralized Simulation Model for Reservoir tem Analysis **HEC NexGen Software Development Project** ues for Applications Developers RAS/HEC-2 Comparison Study -RAS Conveyance Comperison tems Analysis Applications at the rologic Engineering Center off Prediction Uncertainty for Ungauged icultural Watersheds iew of GIS Applications in Hydrologic eling lication of Rainfall-Rumoff Simulation for od Forecasting lication of the HEC Prescriptive Reservoir el in the Columbia River System

REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188				
1a. REPORT SECURITY CLASSIFICATION			1b. RESTRICTIVE MARKINGS					
UNCLASSIFIED 2a. SECURITY CLASSIFICATION AUTHORITY			3 DISTRIBUTION	Y/AVAILABILITY O	FREPORT			
			<u>-</u>	4		-		
126. DECLASSI	FICATION / DOV	WNGRADING SCHEDU	LE					
4. PERFORMI	NG ORGANIZA	TION REPORT NUMBE	R(S)	5. MONITORING ORGANIZATION REPORT NUMBER(S)				
	L PAPER N							
HYDROLOG	IIC ENGINE	ORGANIZATION ERING CENTER	6b. OFFICE SYMBOL (If applicable)	7a. NAME OF MONITORING ORGANIZATION				
	S OF ENGI		CEWRC-HEC	<u> </u>				
	(City, State, and	-		7b. ADDRESS (Ci	ity, State, and ZIP	Code)		
DAVIS CA								
		···						
8a. NAME OF ORGANIZ	FUNDING/SPO ATION	ONSORING	8b. OFFICE SYMBOL (If applicable)	9. PROCUREMEN	T INSTRUMENT ID	ENTIFICATI	ION NUMBER	
WATER RE	SOURCES S	UPPORT CENTER	CEWRC					
	City, State, and	•		10. SOURCE OF	FUNDING NUMBER	S		
	IILDING # DIR VA 22			PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO.	WORK UNIT ACCESSION NO.	
FI BELVO	IIK VA ZZ	000-5500						
11. TITLE (Inc	lude Security C	lassification)		·*	· · · · · · · · · · · · · · · · · · ·	•		
APPLICAT	ION OF TH	E HEC PRESCRIF	TIVE RESERVOIR	MODEL IN THE	E COLUMBIA R	IVER SY	STEM	
12. PERSONAL	AUTHOR(S)							
			AND DAVID FORD)				
			14. DATE OF REPORT (Year, Month, Day) 15. PAGE COUNT MAY 1993					
	NTARY NOTA			MAT 1775			17	
17.	COSATI		18. SUBJECT TERMS (-	-	-	
FIELD	GROUP	SUB-GROUP	SYSTEM ANALYSI NETWORK-FLOW P	•	•		-	
			OPERATING RULE	•	UPERALIUM 31	UDIES,	KESEKVUIK	
			and identify by block n	umber)		· · · · · · · · · · · · · · · · · · ·		
This pap	er summar	izes the inter	rim findings of	the second p	phase of the	HEC-PR	RM Columbia River	
			esents the Colum timize, in time					
			nal goals in HEC					
and ener	gy econom	ic penalty fur	nctions. Operat	ional purpos	ses represen	ted by	penalty functions	
			oly, flood contr					
	fish. The application was based on fifty year period-of-record with a monthly time interval. The HEC data storage system, HEC-DSS, was utilized extensively for data management and							
'analysis of results.								
20 DISTRIBUT	ION/AVAII ARI	LITY OF ABSTRACT		21 ARSTRACT SE	CURITY CLASSIFICA	TION		
		ED SAME AS R	PT. DTIC USERS	II. MUSIRACE SE	_	· · · · · · · ·		
	RICHARD J. HAYES, Hydraulic Engineer				Include Area Code			
RICHARD	J. HAYES,	Mydraulic End	ineer	(916) 756-1	1104	CEWRO	-HEC	